

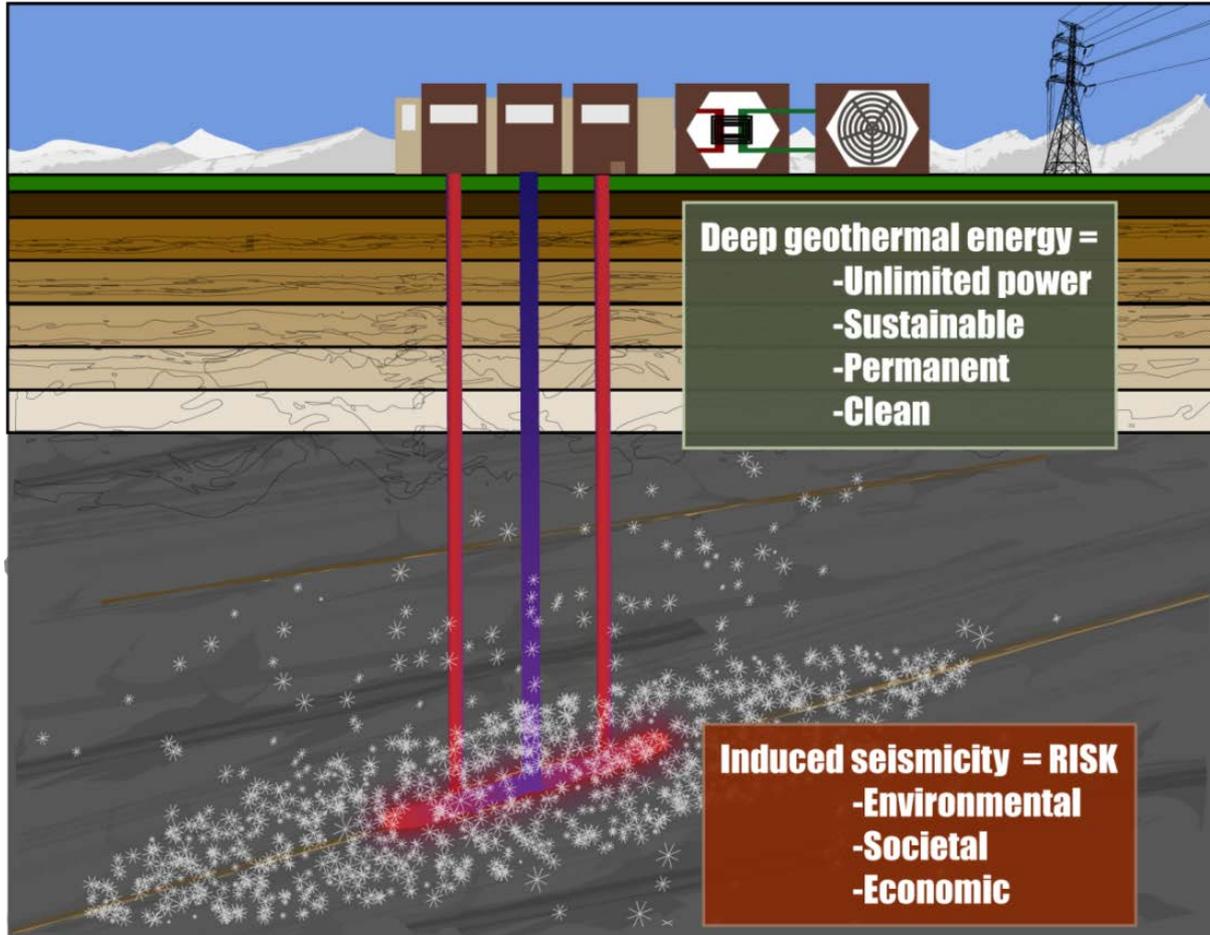
Rock and fluid thermodynamics control the dynamics of induced earthquakes

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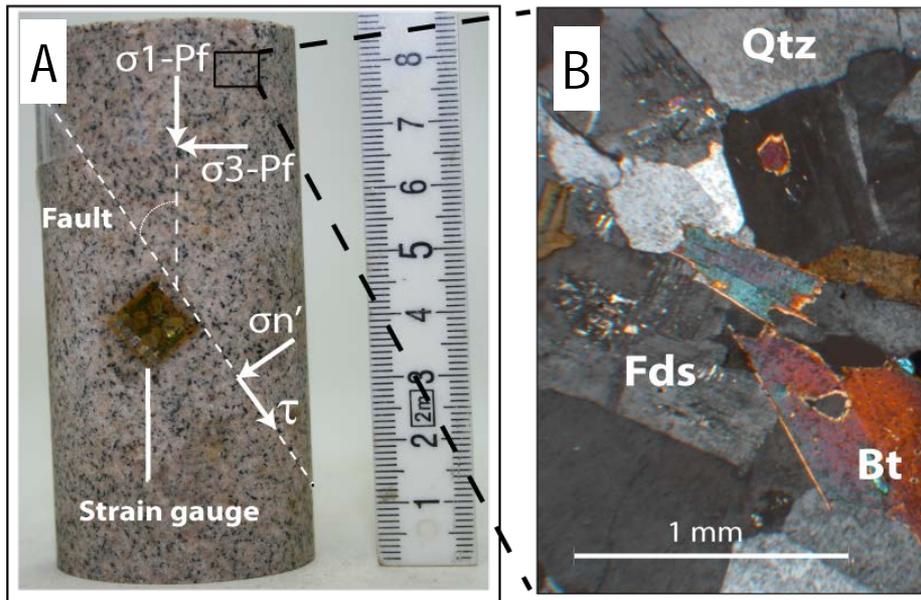
Context – Induced Seismicity in Enhanced Geothermal Systems



UNDERSTAND THE MICROPHYSICAL INTERACTIONS BETWEEN PORE FLUID AND RESERVOIR FAULTS DURING INDUCED EARTHQUAKES

Stick-Slip experiments under Triaxial stress conditions

$$\sigma_1 > \sigma_2 = \sigma_3$$



➤ Samples:

30 ° Saw cut westerly granite cylinders
($\varphi=40$ mm ; H=88 mm)

➤ Instrumentation:

- **External measurements:**

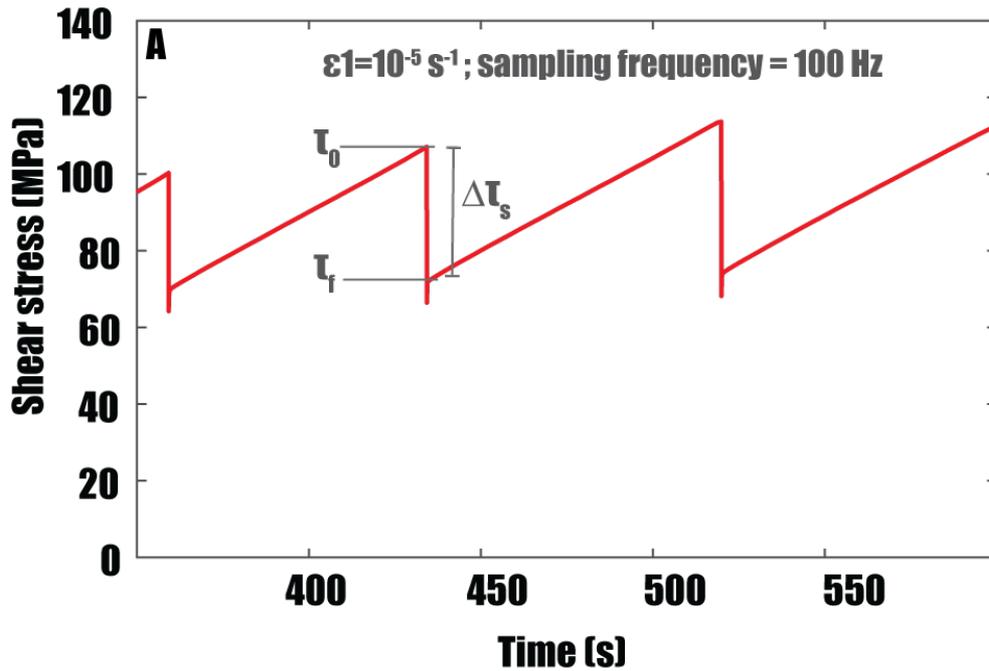
$$\sigma_1 ; \sigma_3 ; p_f ; \epsilon_1$$

- **Internal sensors:**

Near fault strain gauges

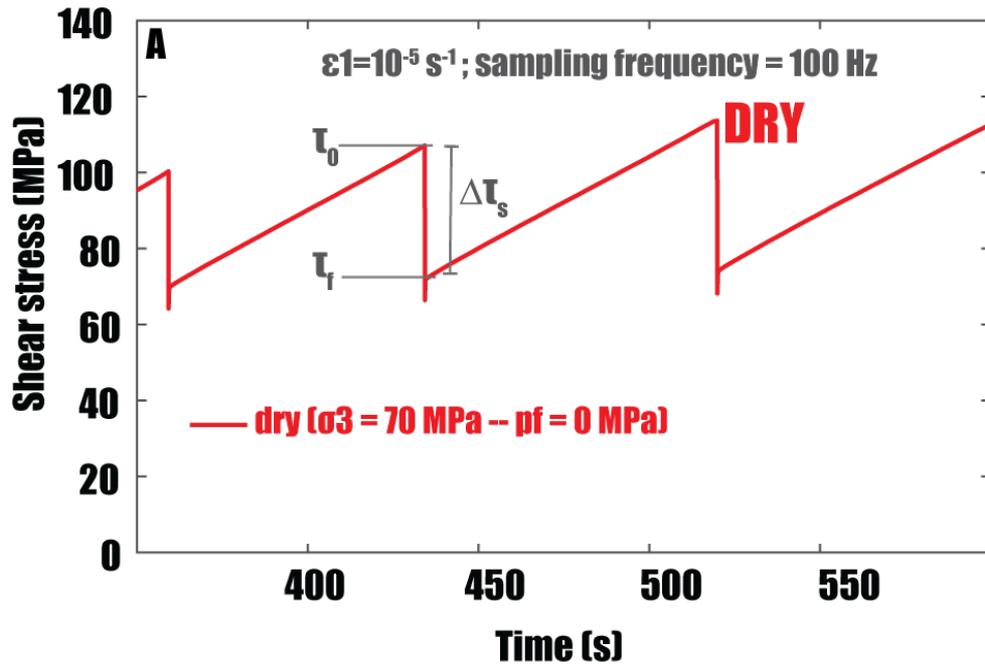
Best analogue for earthquakes

Methods- Stick-slip experiments



Elastic loading until shear strength is reached

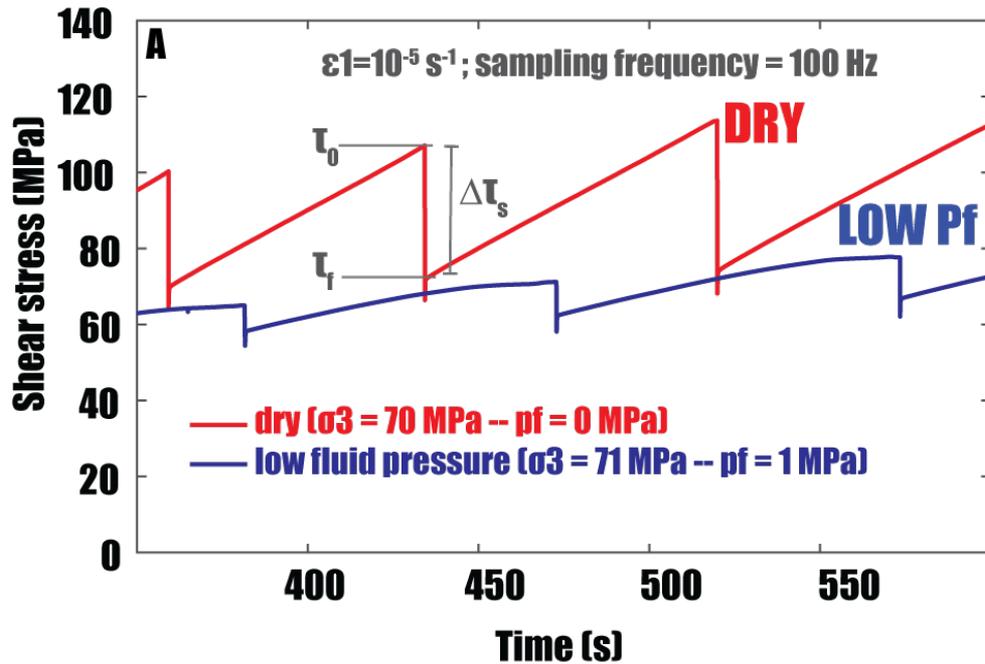
Results- 100 Hz measurements



$P_{\text{ceff}} = P_c - P_f = 70 \text{ MPa}$
 P_f held constant during experiment

Three pore pressure configurations (**DRY**, **Low Pf**, **High Pf**)

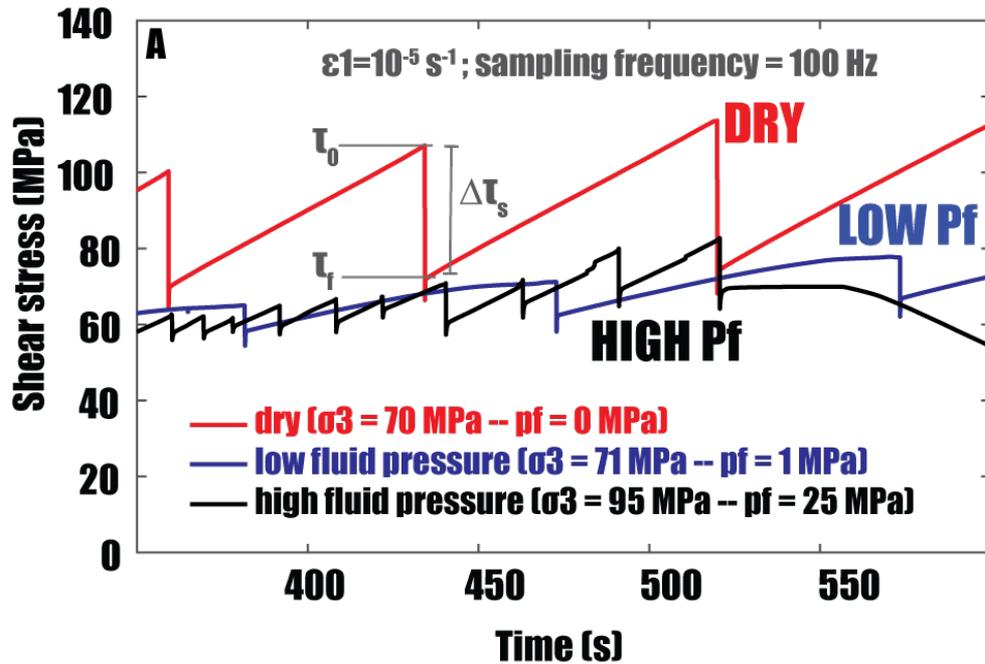
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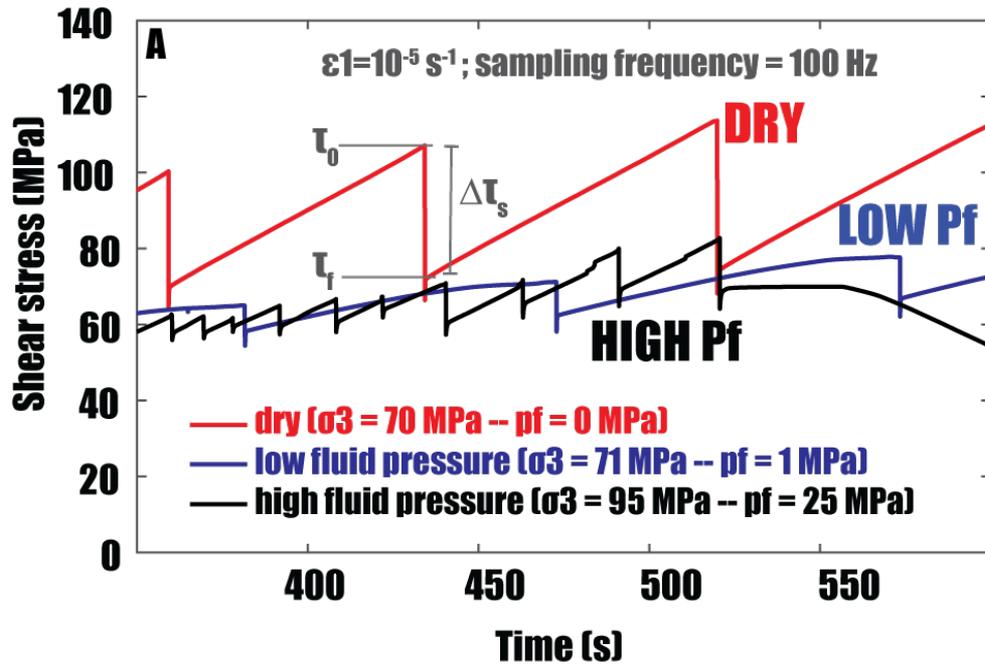
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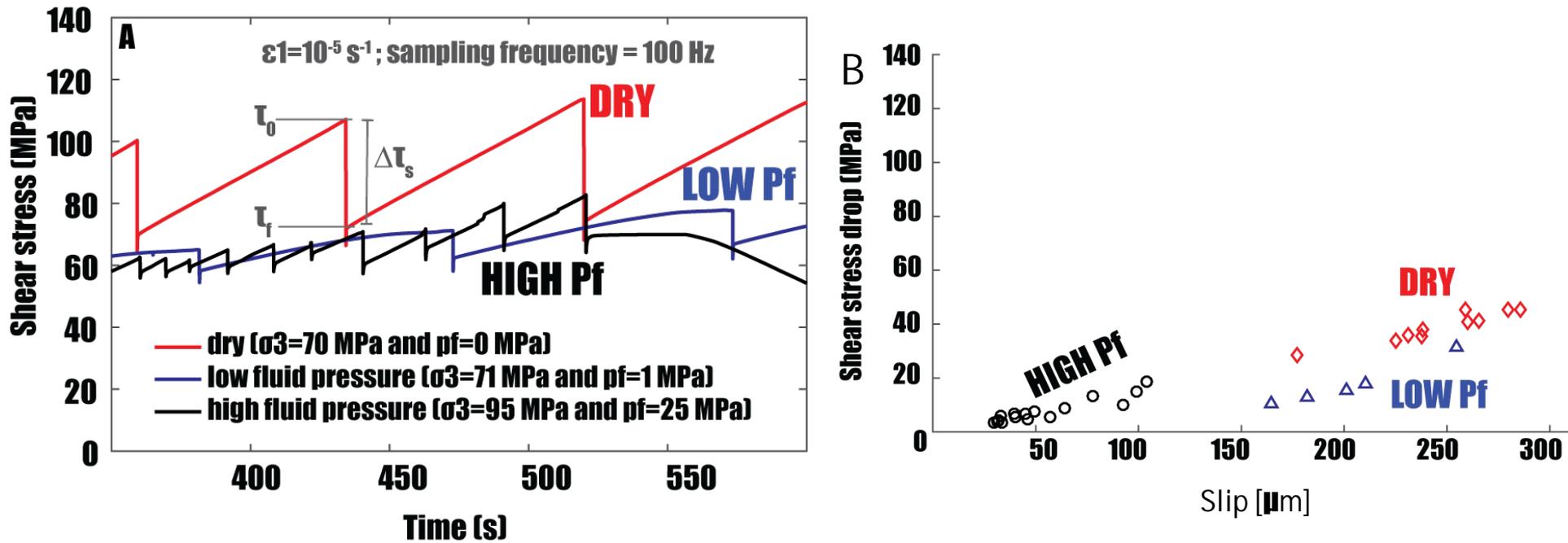


**Water Pressure
==
Lower coulomb
strength.**

$P_{ceff} = P_c - P_f = 70 \text{ MPa}$
 P_f held constant during experiment

Three pore pressure configurations (**DRY**, **Low Pf**, **High Pf**)

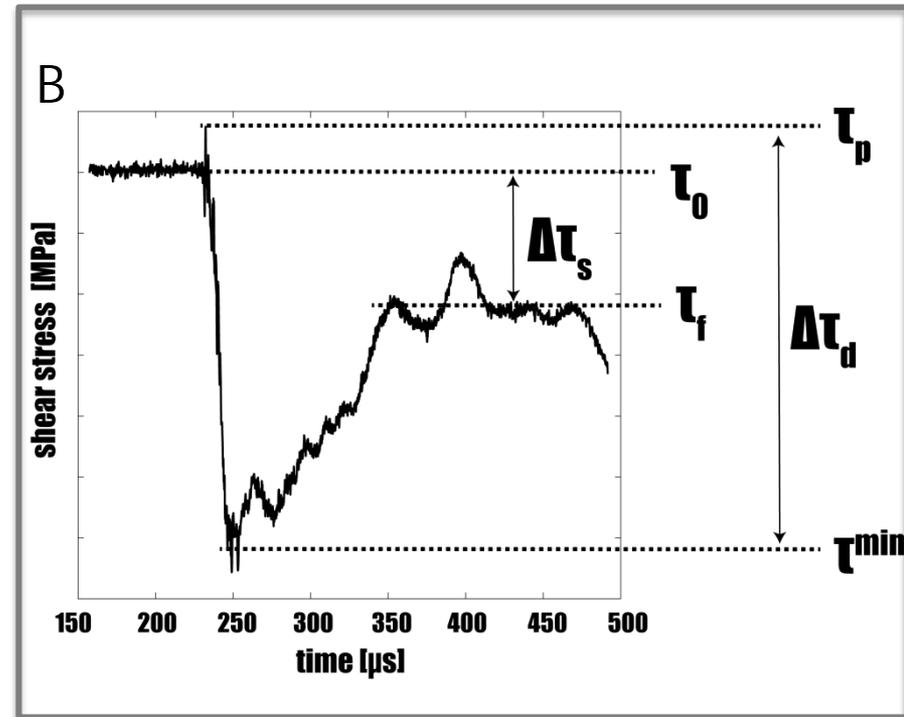
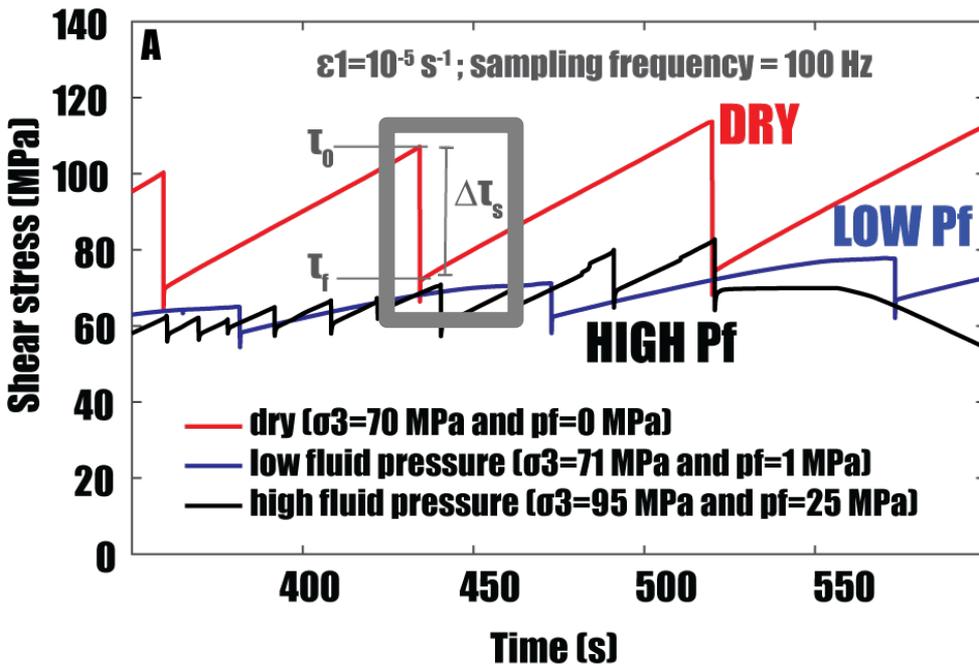
Results- Static stress drop .Vs. Slip



$P_{\text{ceff}} = P_c - P_f = 70 \text{ MPa}$
 P_f held constant during experiment

Pore pressure = low static stress drops

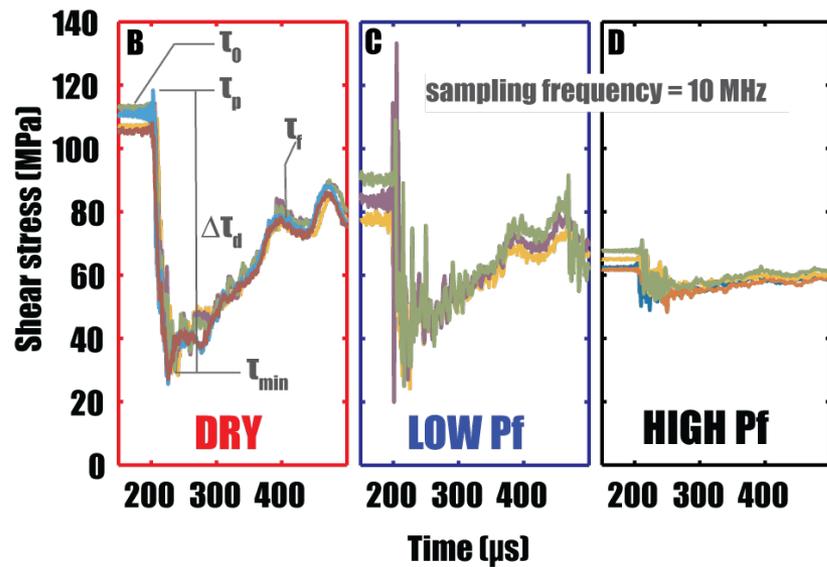
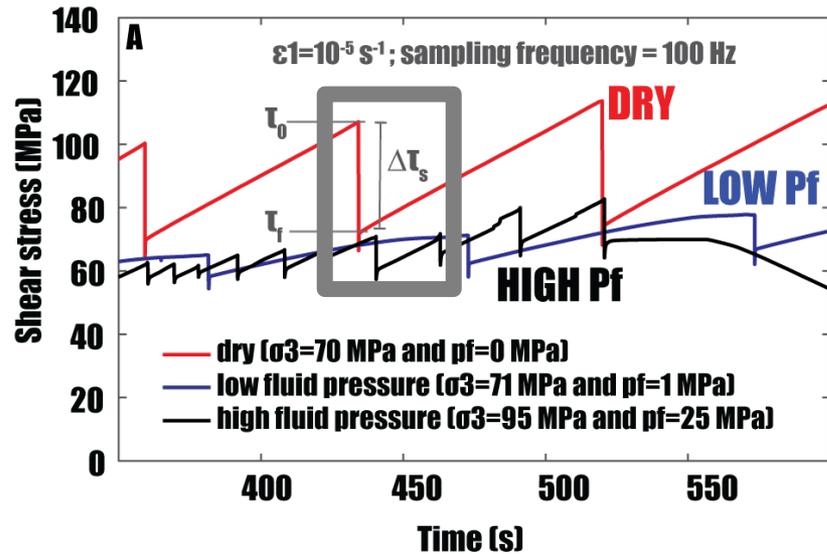
Results – Dynamic stress drop



$P_{\text{ceff}} = P_c - P_f = 70 \text{ MPa}$
 P_f held constant during experiment

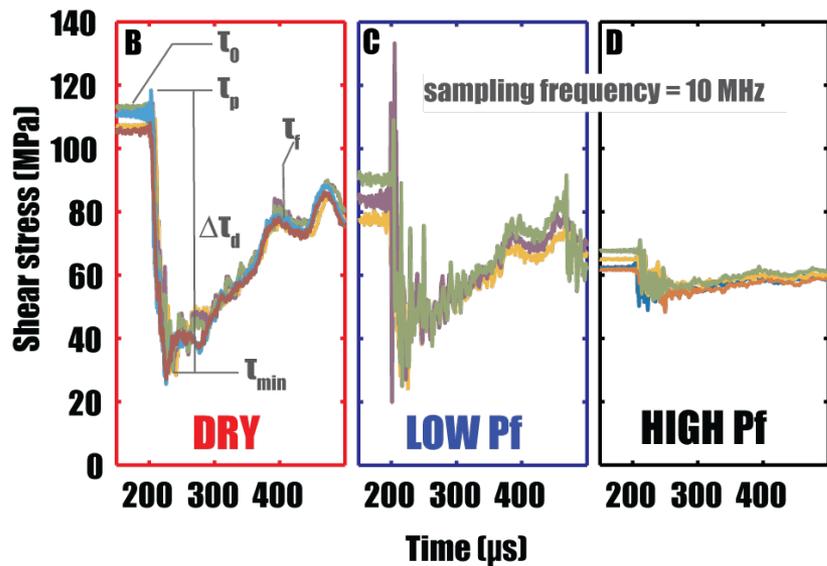
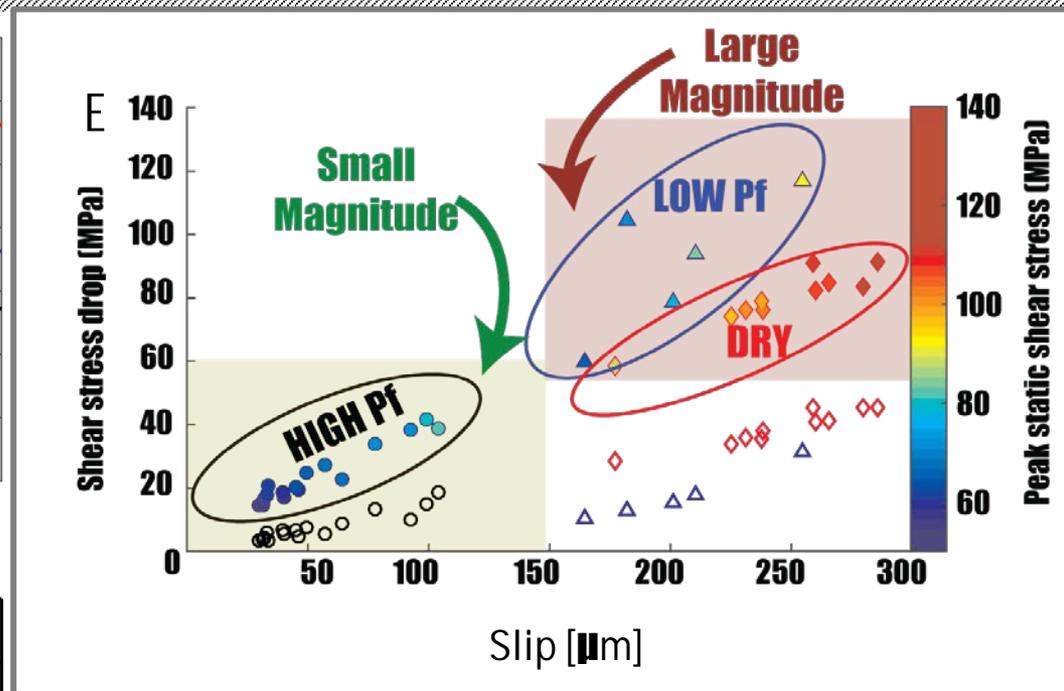
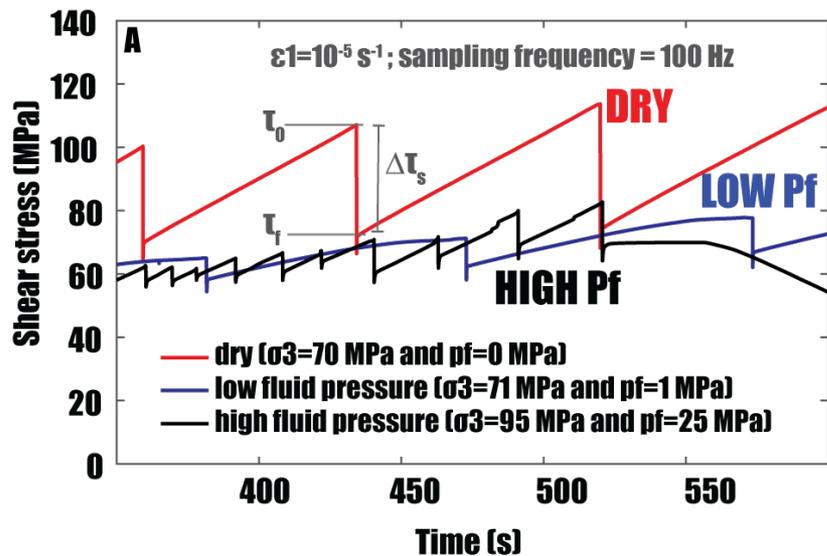
Dynamic recording of near fault stress

Results – Dynamic stress drop



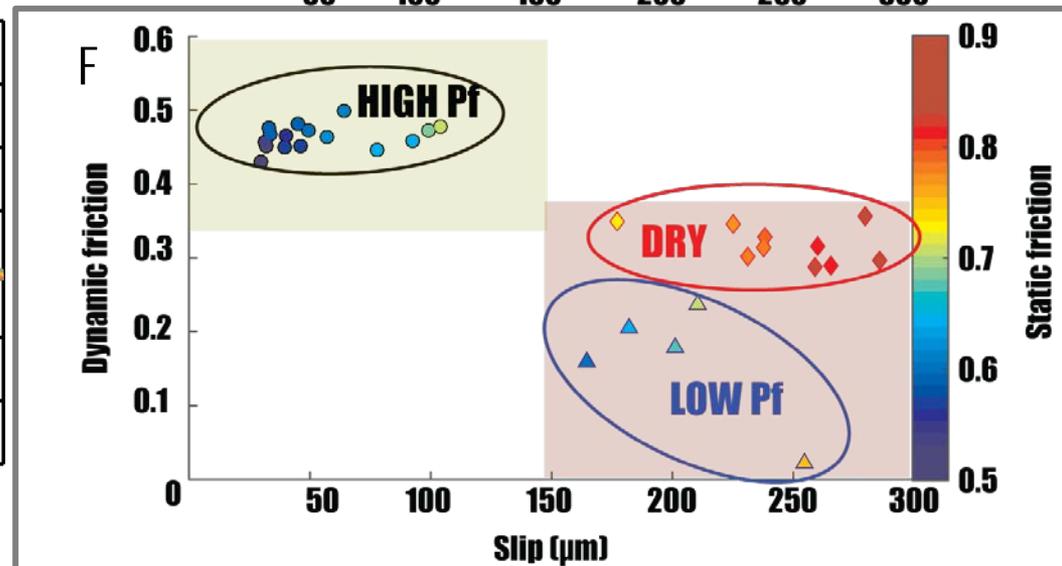
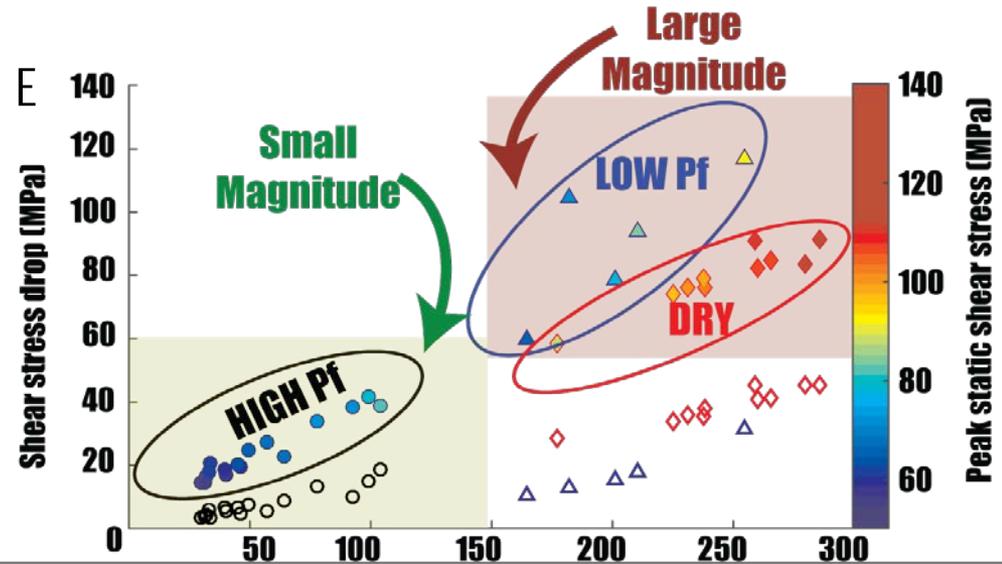
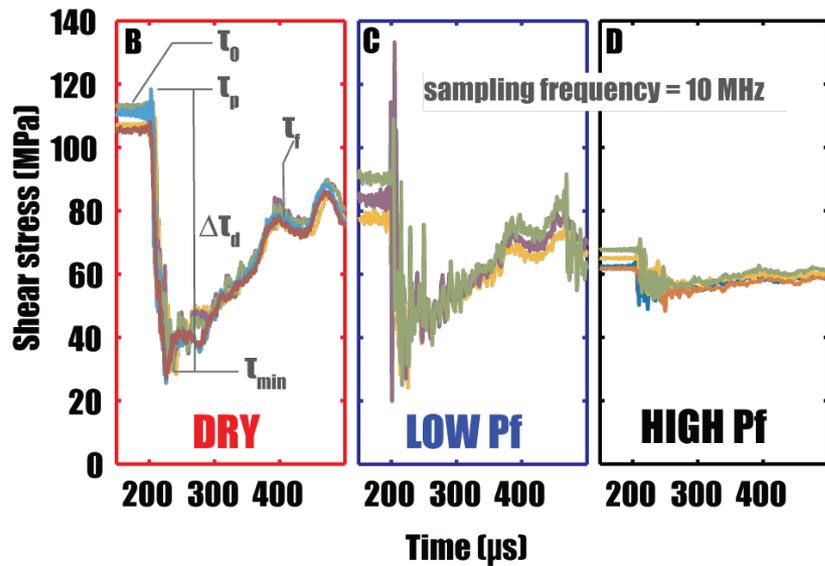
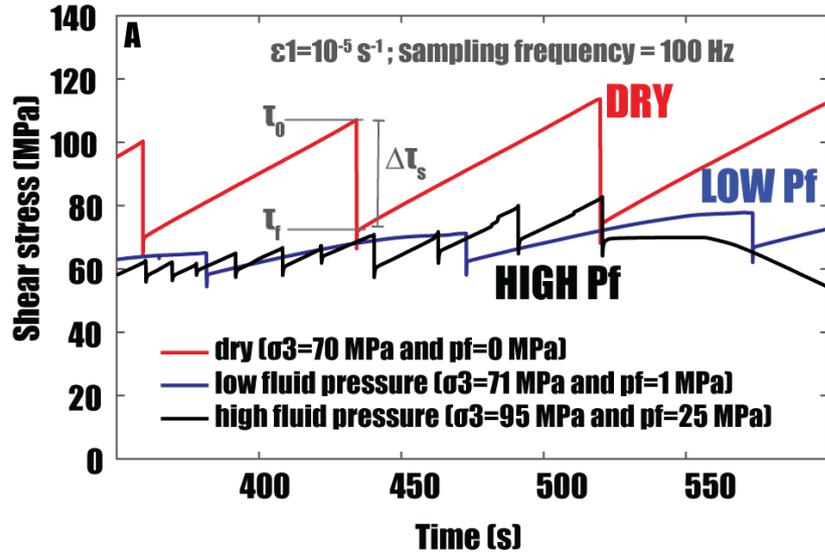
1 curve = 1 dynamic event

Results – Dynamic stress drop .Vs. Slip

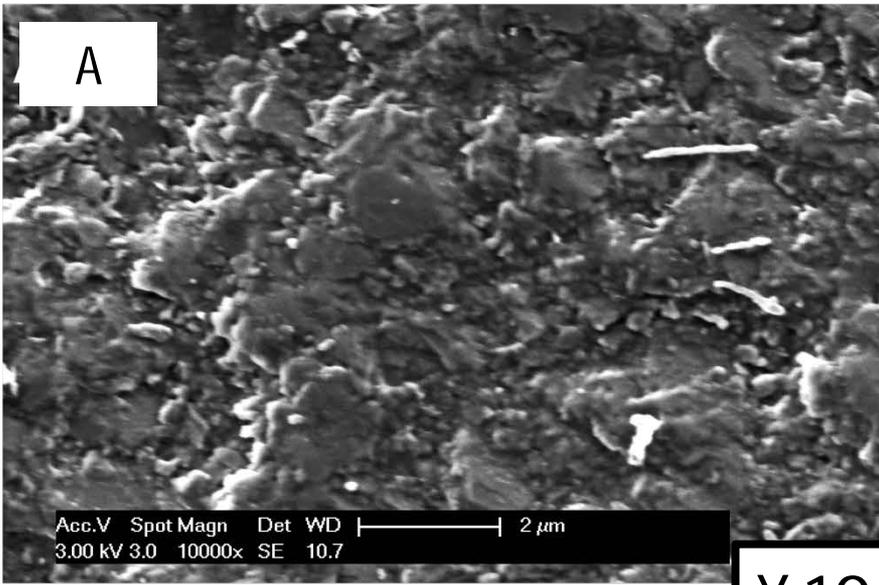


Largest dynamic stress drops at **Low Pf**

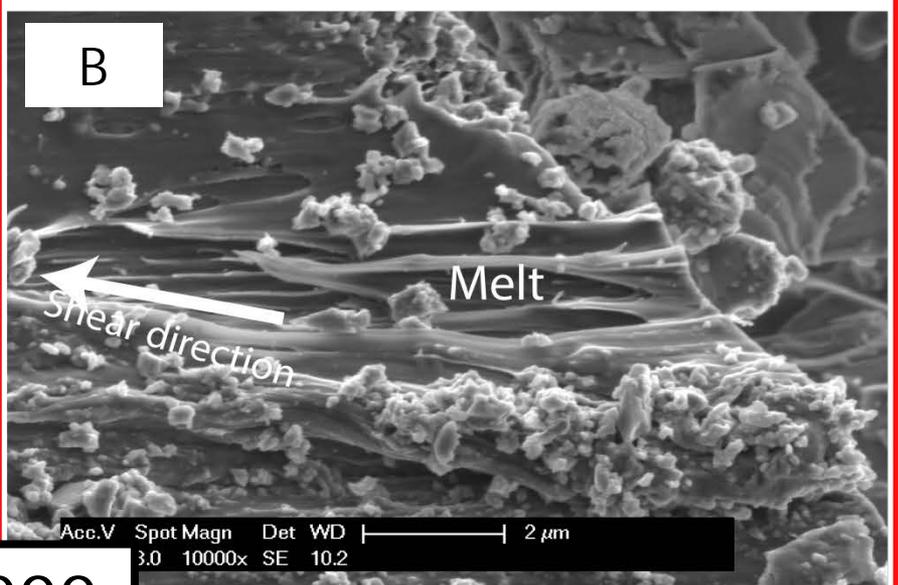
Results – Dynamic Friction



Undeformed material

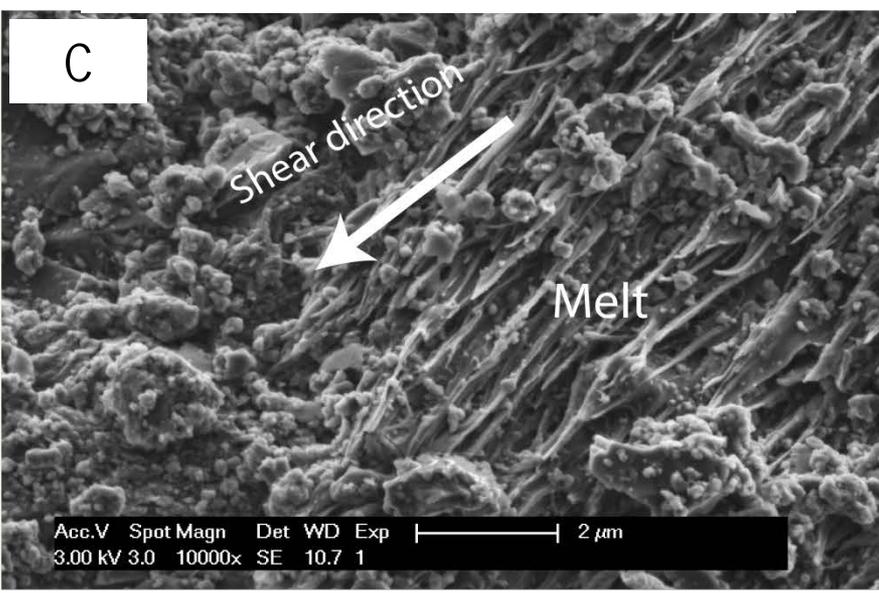


DRY

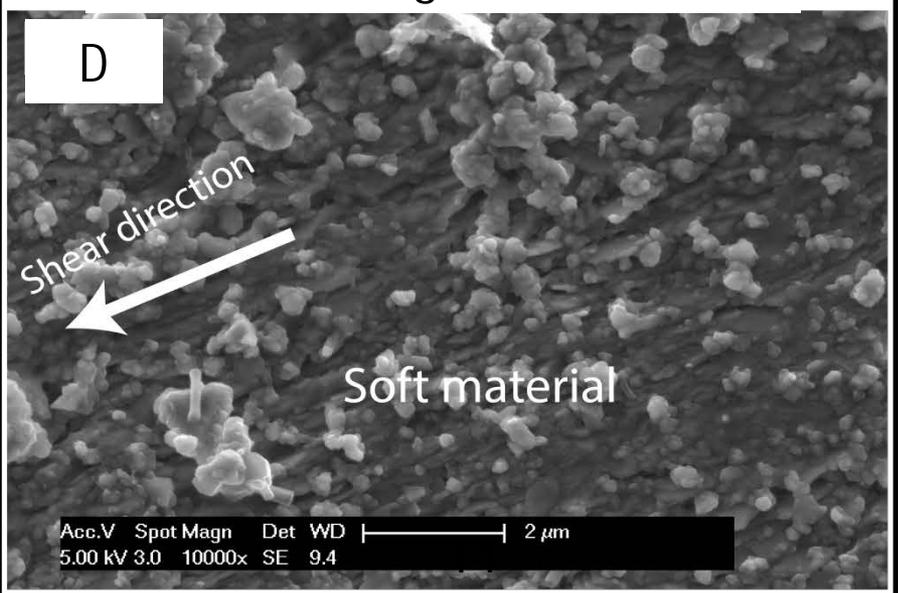


X 10 000

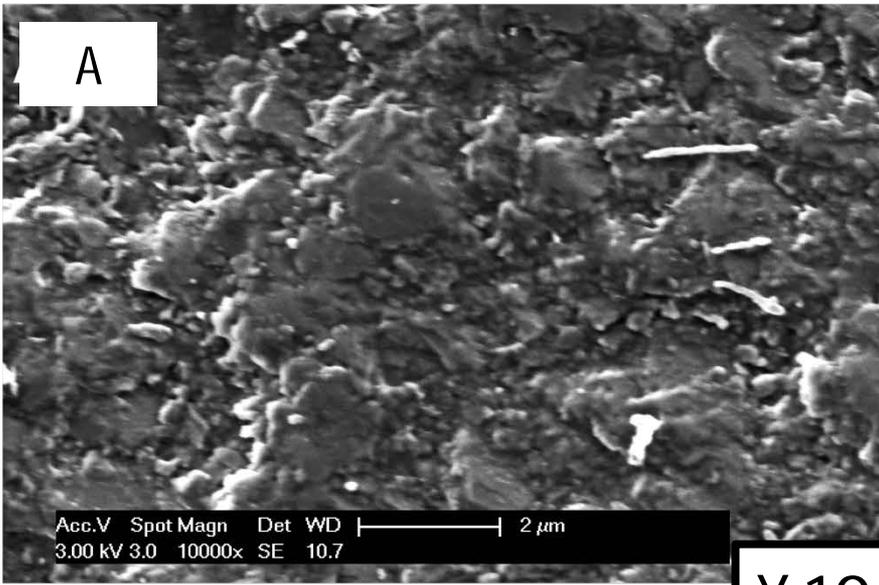
Low Pf



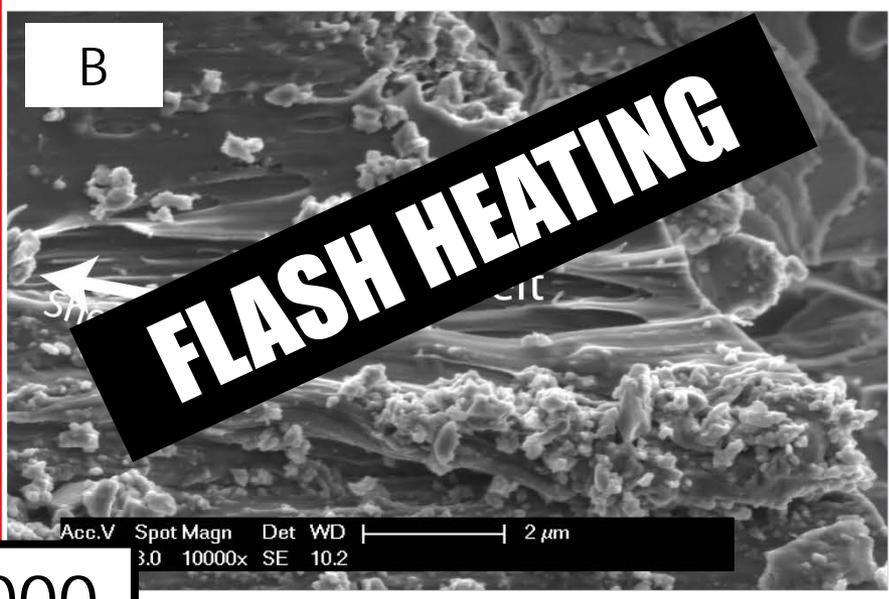
High Pf



Undeformed material

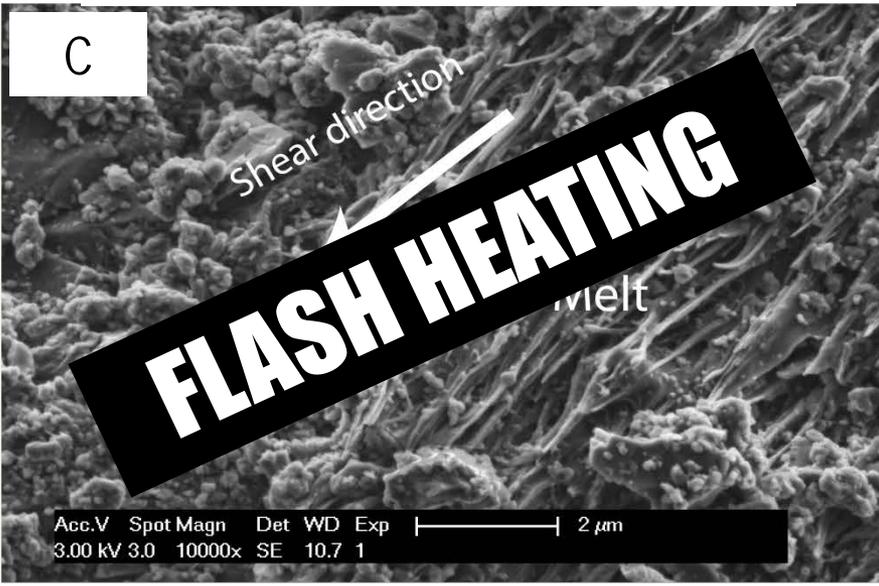


DRY

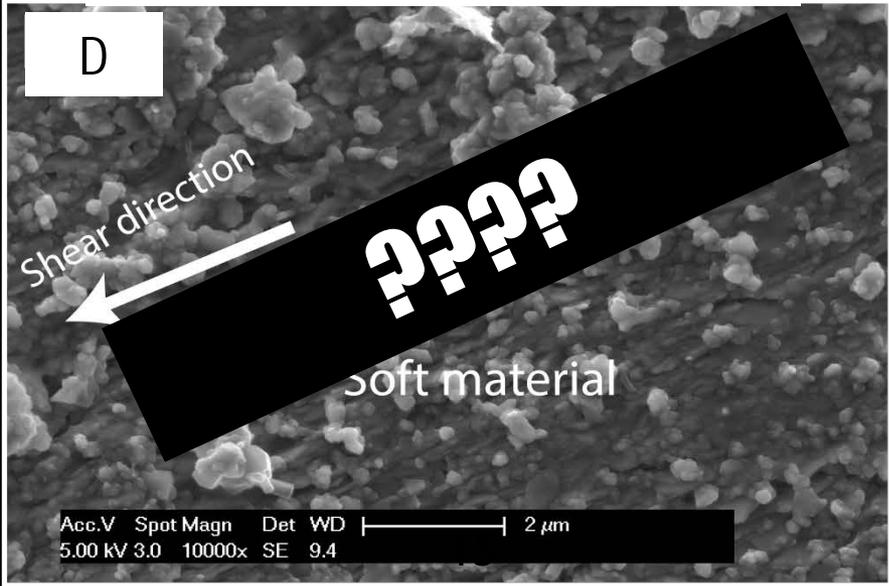


X 10 000

Low Pf

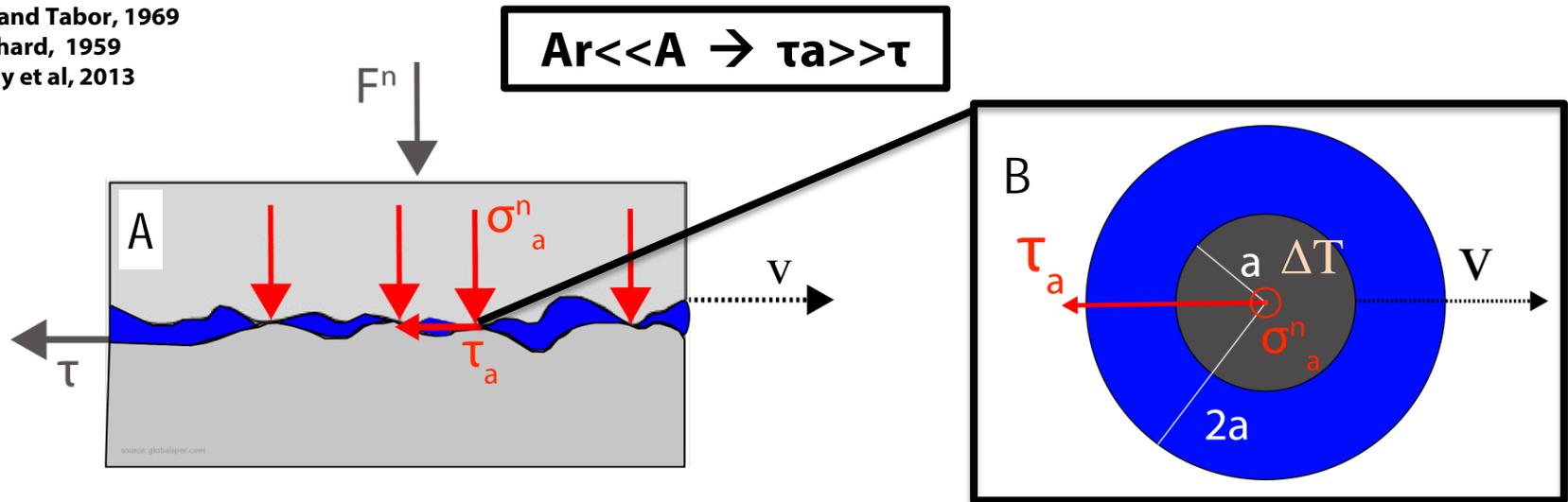


High Pf



Asperity temperature model - Description

Bowden and Tabor, 1969
 Archard, 1959
 Violay et al, 2013



$$\Delta T = f(\tau_a, v) - g(T, \rho_w(P, T), C_{pw}(P, T))$$

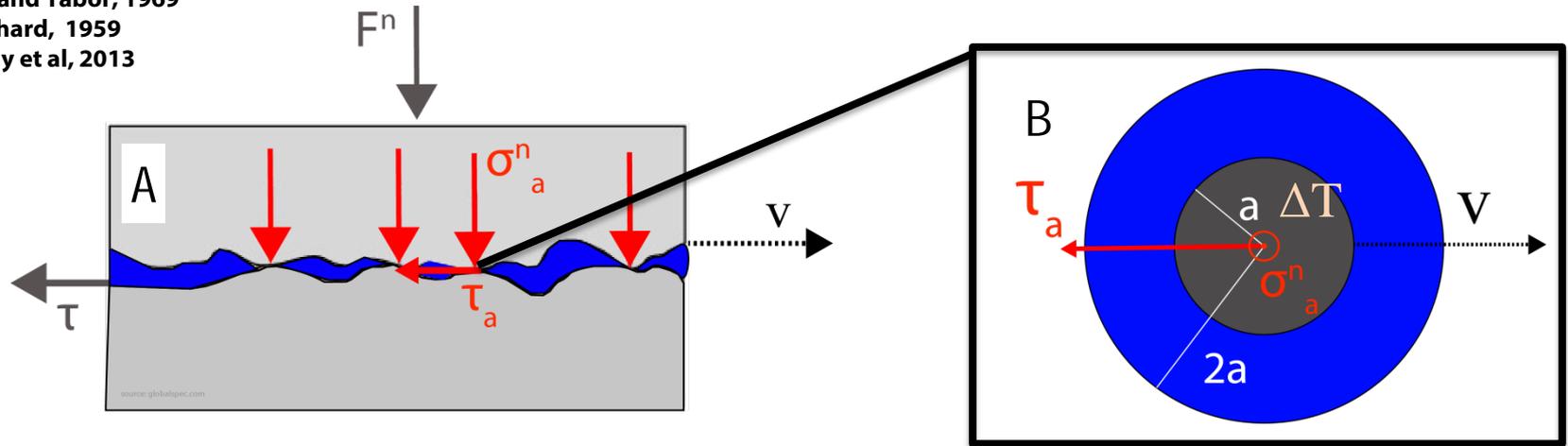
Heat source rate

Temperature buffering

Flash Temperature = maximum transient temperature responsible for weakening

Asperity temperature model - Description

Bowden and Tabor, 1969
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$$\Delta T = f(\tau_a, v) - g(T, \rho_w(P, T), C_{pw}(P, T))$$

Heat source rate

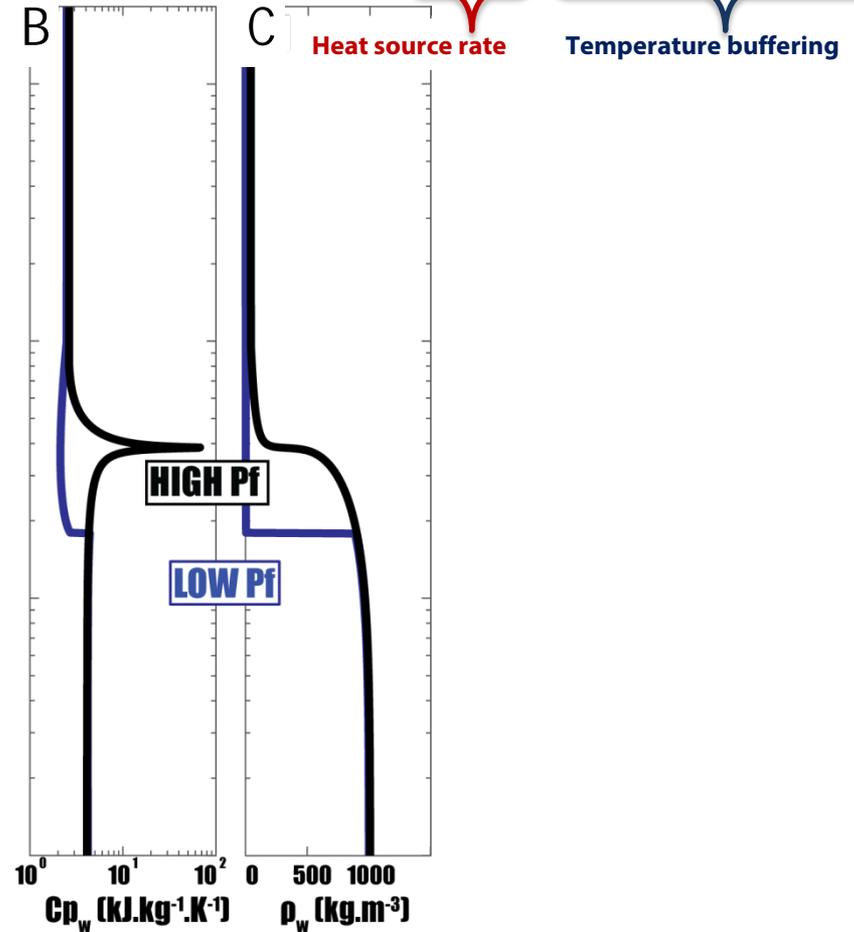
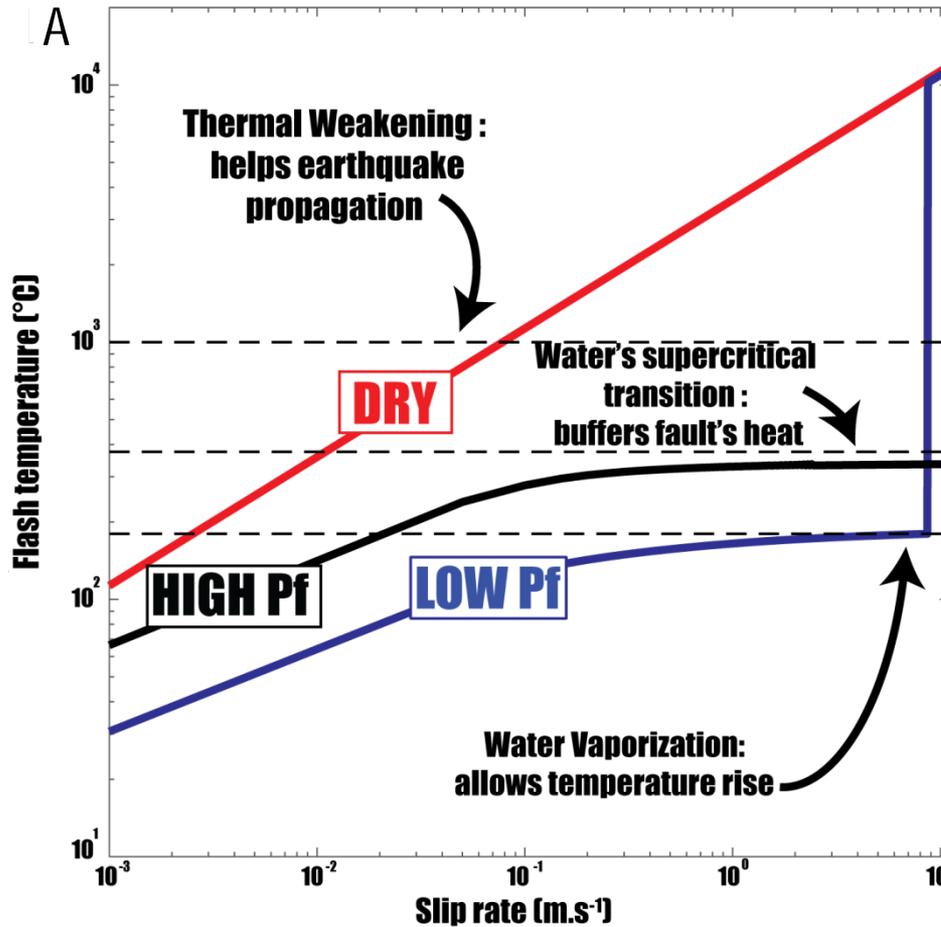
Temperature buffering

Dependence on P & T!

Thermophysical properties of fluid depend on Pressure & Temperature

Asperity temperature model - Results

$$\Delta T = \frac{1}{\rho_{Qz} C_{pQz} \sqrt{k\pi}} \left(\underbrace{\tau_a v \sqrt{t_c}}_{\text{Heat source rate}} - \underbrace{\frac{V_w \rho_w}{t_c \pi a^2} (T C_{pw} + L_w) \sqrt{t_c}}_{\text{Temperature buffering}} \right)$$



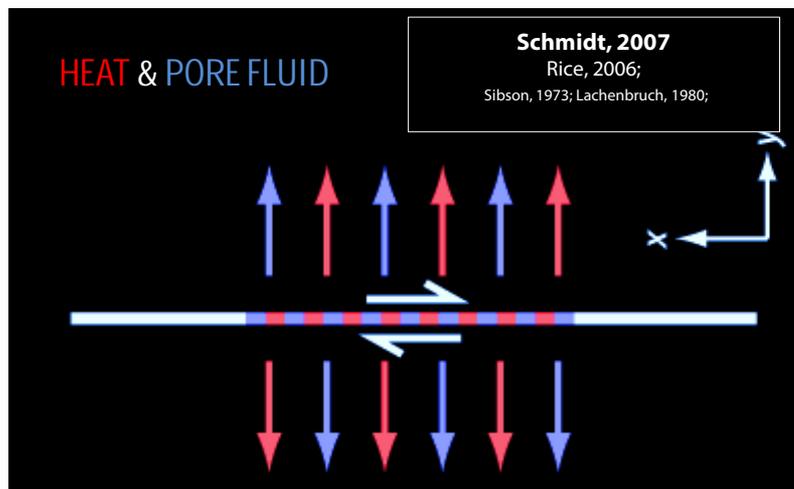
Thermodynamic phase transitions control Temperature rise

Thermal pressurization model

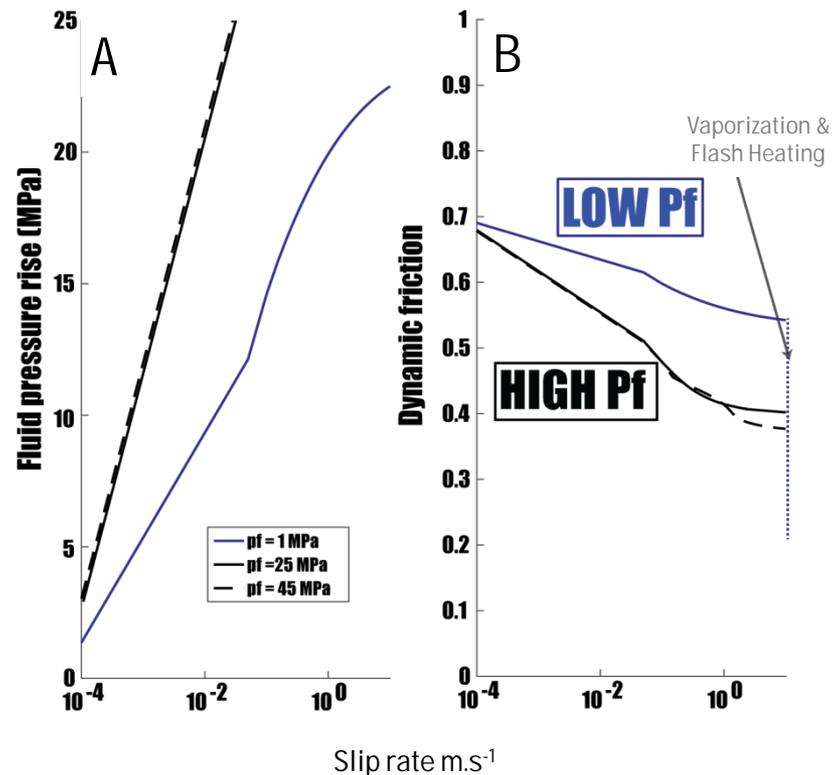
- Difference **DRY** and **LOW Pf** ??

- Stress drop at **HIGH Pf** ??

THERMAL PRESSURIZATION.



$$\Delta p = \frac{\Lambda}{1 + \sqrt{\frac{\alpha_{hyd}}{\alpha_{th}}}} \Delta T \quad \text{Rice, 2006}$$



Thermal pressurization accounts for reduction in dynamic friction

CONCLUSIONS.

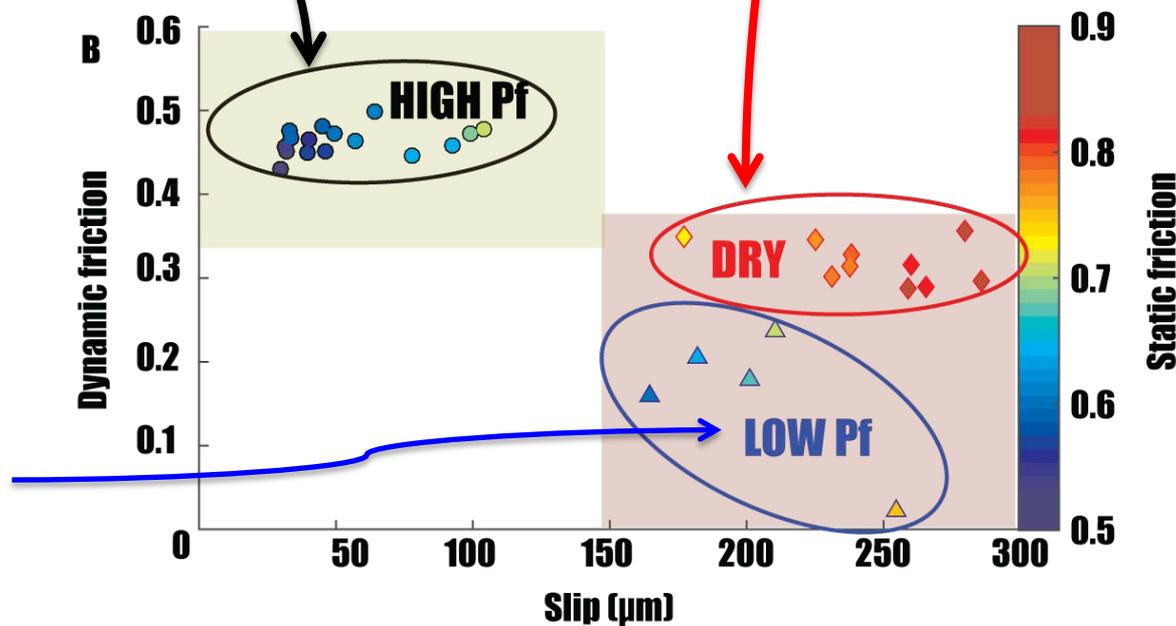
Reduced THERMAL WEAKENING

=
THERMAL PRESSURIZATION

THERMAL WEAKENING

=
FLASH HEATING
(decomposition of contacts)

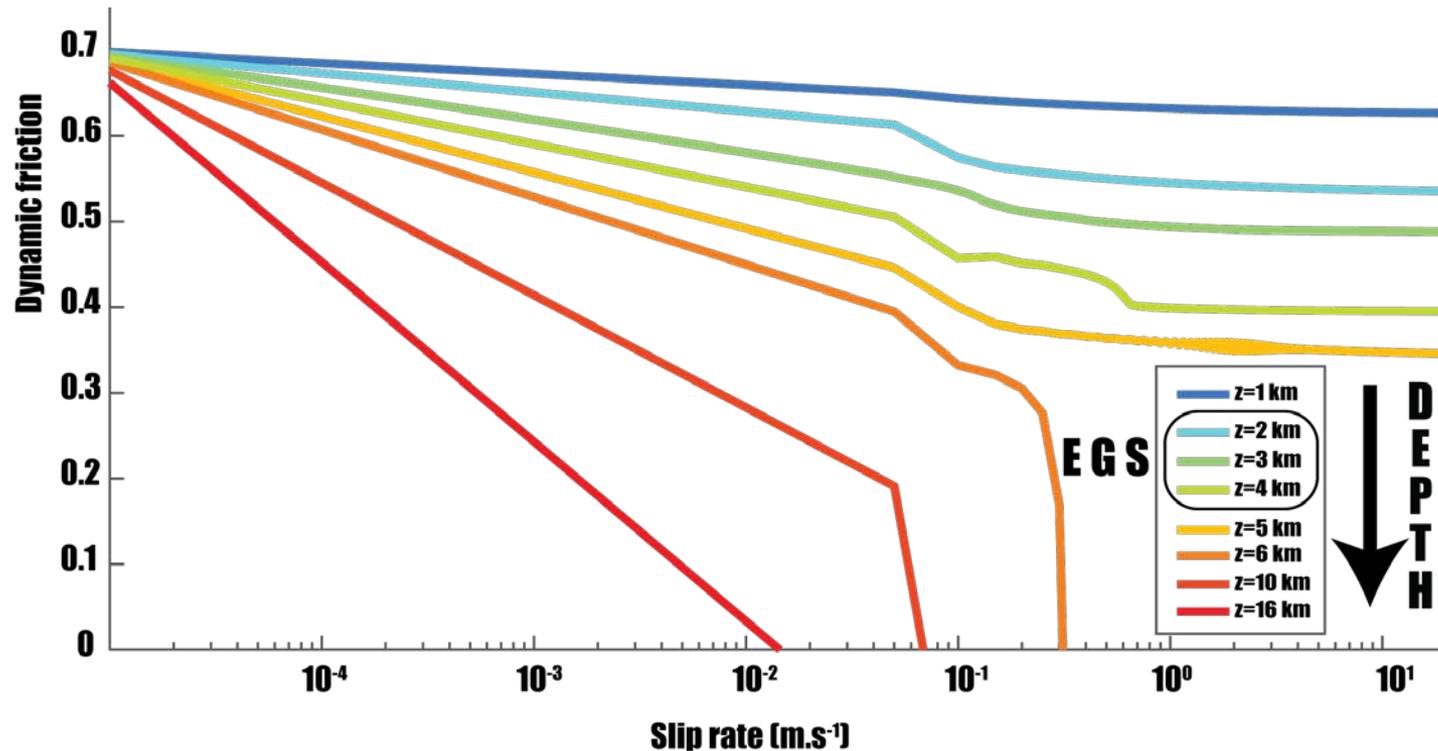
Enhanced THERMAL WEAKENING
=
FLASH HEATING + THERMAL PRESSURIZATION



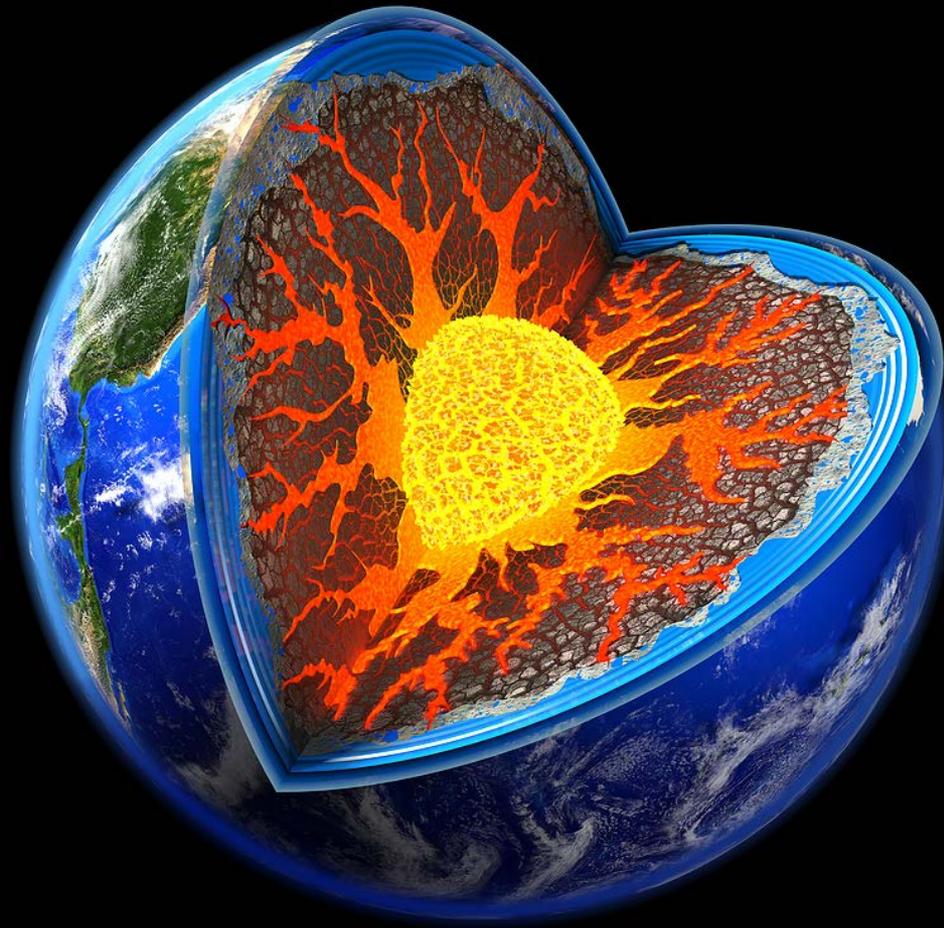
Thermodynamics control dynamic weakening processes during earthquake rupture.

Careful! – σ_N Evolves with depth!

High Depth => Higher stress => FLASH HEATING



Thermophysical properties of water and rock should be taken into account in physics based models



QUESTIONS ?

Asperity temperature model – Parameter description

$$\Delta T = \frac{1}{\rho_{Qz} C_{pQz} \sqrt{k\pi}} \left(\tau_a v \sqrt{t_c} - \frac{V_w \rho_w}{t_c \pi a^2} (T C_{pw} + L_w) \sqrt{t_c} \right)$$

ΔT in $^{\circ}C$ is the temperature rise at the contacting asperities.

v in $m.s^{-1}$ is the slip rate relative to the contacting asperities.

t_c in s is the average contacting time between asperities which is defined as $t_c = \sqrt{\frac{a}{v}}$ by *Rice, 2006*.

τ_a in MPa is the shear stress acting on a single asperity at the onset of instability.

a in m is the average size of asperities defined as $a = \sqrt{\frac{F}{M\pi Pm}}$. Where:

F in N is the normal force applied to the surface.

M is the number of asperities in contact as defined by *Dietrich and Kilgore, 1994* and calculated for our surface.

Pm in Pa the critical yield stress or penetration hardness of Quartz.

ρ_{Qz} in $kg.m^{-3}$, C_{pQz} in $J.kg^{-1}.K^{-1}$ and k in $m^2.s^{-1}$ are respectively the density, specific heat and thermal conductivity of Quartz.

$\rho_w(P, T)$ in $kg.m^{-3}$ and $C_{pw}(P, T)$ in $J.kg^{-1}.K^{-1}$ are respectively the density and specific heat of water.

V_w in m^3 is water volume interacting with asperities during shear heating defined in the same manner as *Violay et al, 2013* over a thickness of $100 \mu m$.